

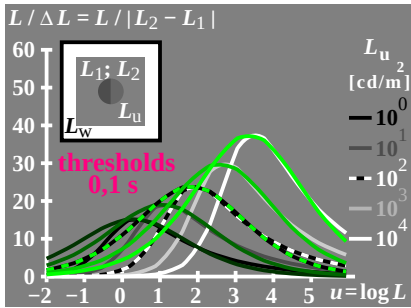
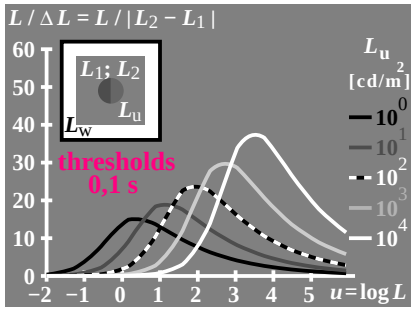
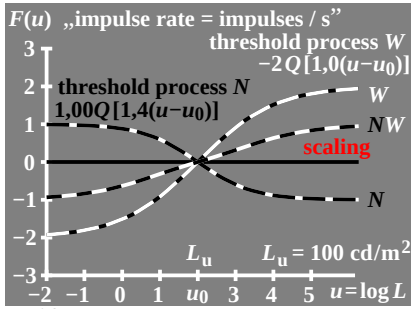
Weber-Fechner law in CIE 230:2019 for threshold colour differences of surface colours

The Weber-Fechner law describes the lightness L^* as **logarithmic** function of L_r .
The Stevens law describes the lightness L^* as **potential** function of $L_r = Y/5$.
IEC 61966-2-1 uses a similar potential function $L_{TIC} = m L_r^{1/2.4}$.
The Weber-Fechner law is equivalent to the equation: $\Delta L_r = c L_r$ [1]
Integration leads to the logarithmic equation: $L^* = k \log(L_r)$ [2]
Derivation for $\Delta L_r = 1$ leads to the linear equation: $L_r / \Delta L_r = k = 57$ [3]
For colours in offices the **standard contrast range** is 25:1=90:3.6

Table 1: CIE tristimulus value Y , luminance L , and lightness L^*

Colour (matte)	Tristimulus value Y	office luminance L [cd/m ²]	relative luminance $L_r = L/L_u$	CIE lightness $L^*_{CIELAB} \sim m L_r^{1/2.4}$	relative lightness $L^*_r = k \log(L_r)$
White W (paper)	90	142	5	94	44
Grey Z (paper)	18	28,2	1	50	0
Black N (paper)	3,6	5,6	0,2	18	-40

For the lightness range between $L^*_r = -40$ and 40 the constant is: $k = 40/\log(5) = 57$



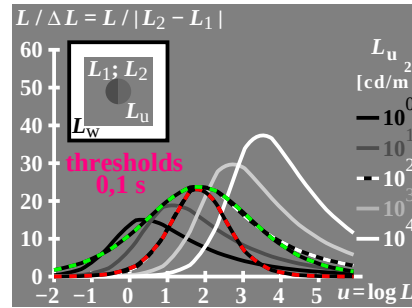
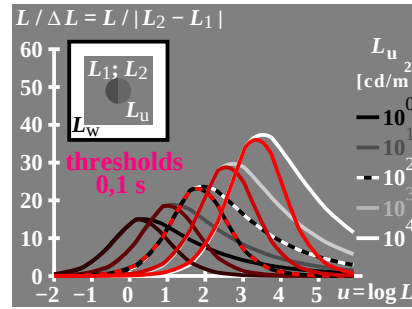
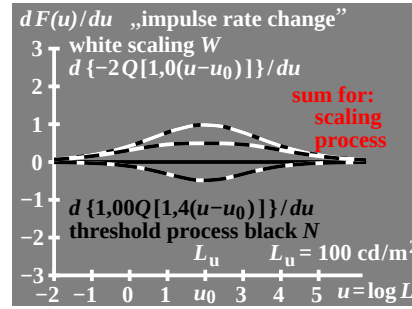
Weber-Fechner law in CIE 230:2019 for threshold colour differences of surface colours and two ranges $0.2 < L_r < 1$ and $1 < L_r < 5$

The Weber-Fechner law describes the lightness L^* as **logarithmic** function of L_r .
The Stevens law describes the lightness L^* as **potential** function of $L_r = Y/5$.
IEC 61966-2-1 uses a similar potential function $L_{TIC} = m L_r^{1/2.4}$.
The Weber-Fechner law is equivalent to the linear equation: $\Delta L_r = c L_r$ ($c=0.1$) [1]
Integration leads to the logarithmic equation: $L^* = k_1 \log(L_r)$ ($c=0.1$) [2]
Derivation for $\Delta L_r = 1$ leads to the linear equation: $L_r / \Delta L_r = k_1$ ($k_1=46$, $k_1=63$) [3]
For colours in offices the **standard contrast range** is 25:1=90:3.6

Table 1: CIE tristimulus value Y , luminance L , and lightness L^*

Colour (matte)	Tristimulus value Y	office luminance L [cd/m ²]	relative luminance $L_r = L/L_u$	CIE lightness $L^*_{CIELAB} \sim m L_r^{1/2.4}$	relative lightness $L^*_r = k \log(L_r)$
White W (paper)	90	142	5	94	44
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For the two lightness ranges it is $k_0 = -32/\log(0.2) = 46$ and $k_1 = 44/\log(5) = 63$.



line element of Stiles
(1946) with „color values” L_P, M_D, S_T
three separate color signal functions
 $F(L_P) = i \ln(1 + 9 L_P)$
 $F(M_D) = j \ln(1 + 9 M_D)$
 $F(S_T) = k \ln(1 + 9 S_T)$
Taylor-derivations:
 $\Delta F(L_P, M_D, S_T) = \frac{dF}{dL_P} \Delta L_P + \frac{dF}{dM_D} \Delta M_D + \frac{dF}{dS_T} \Delta S_T$
 $= \frac{9i}{1+9L_P} \Delta L_P + \frac{9j}{1+9M_D} \Delta M_D + \frac{9k}{1+9S_T} \Delta S_T$

functions $q[k(u-u_0)]$
„achromatic signal”-description
with $u = \log L$ (L = luminance)
 $u_0 = \log L_u$ (L_u = surround luminance)
 $q[k(u-u_0)] = 1 + 1/[1 + \sqrt{2} e^{k(u-u_0)}]$
function values:
 $q[k(u-u_0) \rightarrow +\infty] = 1$
 $q[k(u-u_0) = 0] = \sqrt{2}$
 $q[k(u-u_0) \rightarrow -\infty] = 2$

„achromatic signal” discrimination
as function of relative light density
 $h = \ln H = k(u-u_0)$, $\ln$ = natural log.
 $Q' = \frac{d}{dH} [\ln\{1 + 1/(1 + \sqrt{2} H)\}] / \ln \sqrt{2}$
 $= -\sqrt{2} / [\ln \sqrt{2} (1 + \sqrt{2} H)(2 + \sqrt{2} H)]$
function values:
 $Q'[k(u-u_0) \rightarrow +\infty] = 0$
 $Q'[k(u-u_0) = 0] = -0,5$
 $Q'[k(u-u_0) \rightarrow -\infty] = 0$

double line element of Richter
(1987) for the lighting technology with the luminance $L = f(L_P, M_D, S_T)$
 $F(L) = \int_{-\infty}^L (L/\Delta L) dL$ (relative lightness?)
 $F(L) = iQ(H) = \begin{cases} iQ(H) & (u < u_0) \\ iQ(\bar{H}) & (u \geq u_0) \end{cases}$
with: $k=1,4$ $\bar{k}=1$ $i=1$ $\bar{i}=-2$
 $u = \log L$ $u_0 = \log L_u$
 $H = e^{k(u-u_0)}$, $\bar{H} = e^{\bar{k}(u-u_0)}$, $\bar{H} = e^{\bar{k}(u-u_0)}$

line element of Vos&Walraven
(1972) with „color values” L_P, M_D, S_T
three separate color signal functions
 $F(L_P) = -2i\sqrt{L_P}$
 $F(M_D) = -2j\sqrt{M_D}$
 $F(S_T) = -2k\sqrt{S_T}$
Taylor-derivations:
 $\Delta F(L_P, M_D, S_T) = \frac{dF}{dL_P} \Delta L_P + \frac{dF}{dM_D} \Delta M_D + \frac{dF}{dS_T} \Delta S_T$
 $\Delta F(L_P, M_D, S_T) = \frac{i}{\sqrt{L_P}} \Delta L_P + \frac{j}{\sqrt{M_D}} \Delta M_D + \frac{k}{\sqrt{S_T}} \Delta S_T$

„achromatic signal”-description
functions $Q_{1m}[k(u-u_0)]$
with $u = \log L$ (L = luminance)
 $u_0 = \log L_u$ (L_u = surround luminance)
 $Q_{1m}[k(u-u_0)] = \frac{l}{\ln \sqrt{2}} \ln q[k(u-u_0)] - m$
function values with $l = m = 1$:
 $Q[k(u-u_0) \rightarrow +\infty] = 1$
 $Q[k(u-u_0) = 0] = 0$
 $Q[k(u-u_0) \rightarrow -\infty] = -1$

luminance discrimination
possibility $L/\Delta L$ as function of H
with: $L = 10^u$ $H = e^h = 10^{\log e k(u-u_0)}$
 $dL/du = \ln 10 L$ $dH/du = k H$
it follows: $L/\Delta L = [kH / (dH \ln 10)]$
 $\frac{L}{\Delta L} = \text{const } H / [(1 + \sqrt{2} H)(2 + \sqrt{2} H)]$
 $Q'[k(u-u_0) \rightarrow +\infty] = 0$
 $Q'[k(u-u_0) = 0] = \text{maximum}$
 $Q'[k(u-u_0) \rightarrow -\infty] = 0$

double line element of Richter
(1987) for the lighting technology with the luminance $L = f(L_P, M_D, S_T)$
 $F(L) = \int_{-\infty}^L (L/\Delta L) dL$ (relative lightness?)
 $F(L) = iQ(H)$ $H = e^{k(u-u_0)}$
 $Q(H) = [\ln\{1 + 1/(1 + \sqrt{2} H)\}] / \ln \sqrt{2} - 1$
Taylor-derivations:
 $\Delta F(L) = \frac{dF}{dL} \Delta L = i \frac{dQ}{dH} \Delta H$
 $= -i\sqrt{2} \Delta H / [\ln \sqrt{2} (1 + \sqrt{2} H)(2 + \sqrt{2} H)]$