



Weber-Fechner law CIE 230:2019 for threshold colour differences of surface colours:

The Weber-Fechner law describes the lightness  $L^*$  as logarithmic function of  $L_r$ . The Weber-Fechner law describes the lightness  $L_{\text{CIELAB}}$  as potential function of  $L_r=L^*/100$ . IEC 61966-2-1 uses a similar potential function  $L_{\text{CIE}}=m \cdot L_r^{1/2.4}$ .

The Weber-Fechner law is equivalent to the equation:  $AL_r=c \cdot L_r$  [1]

Integration leads to the logarithmic equation:  $L^*=k \log(L_r)$ , [2]

Derivation for  $AL_r=1$  leads to the linear equation:  $L_r/\Delta L_r=k=57$ . [3]

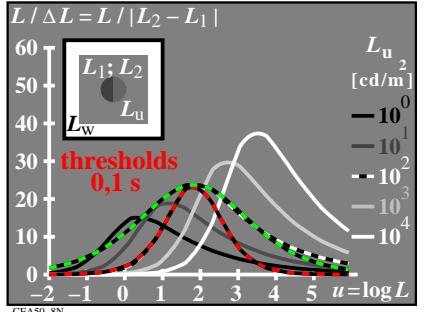
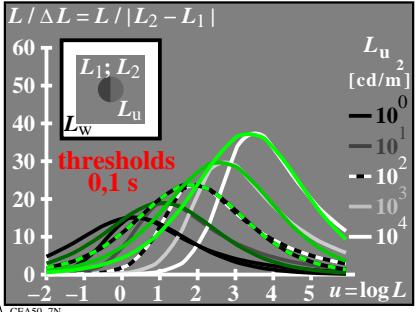
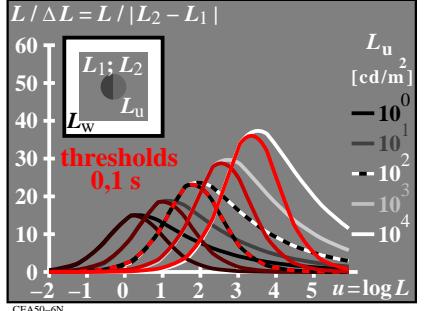
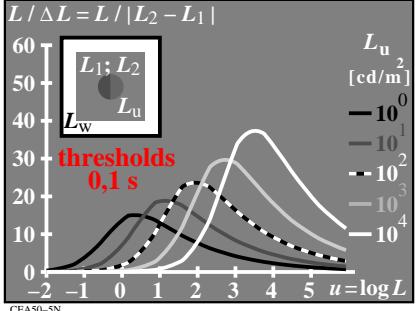
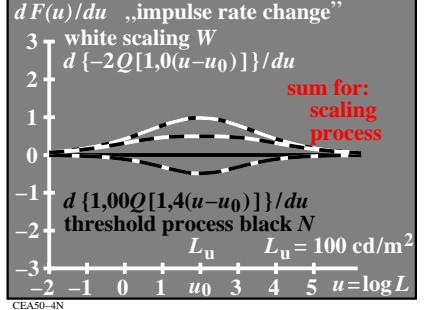
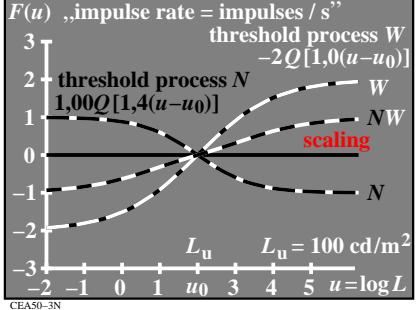
For colours in offices the standard contrast range is 25:1-90:3.6.

Table 1: CIE tristimulus value Y, luminance L, and lightnesses L\*

Colour (matte)	Tristimulus value Y	office luminance	relative luminance	CIE lightness	relative lightness
(contrast) 25:1-90:3.6)	$L$ [cd/m <sup>2</sup> ]	$L_r=L/L_u$	$L^*_{\text{CIELAB}}$ $=m \cdot L_r^{1/2.4}$	$L^*$	$=k \log(L_r)$
White W (paper)	90	142	5	94	40
	$\approx 18^{\circ}5$	$\approx 28.2^{\circ}5$		$\approx 50+44$	$=k \log(5)$
Grey Z (paper)	18	28.2	1	50	0
Black N (paper)	3.6	5.6	0.2	18	-40
	$\approx 18^{\circ}5$	$\approx 28.2^{\circ}5$		$\approx 50-32$	$=k \log(0.2)$

For the lightness range between  $L^*=40$  and  $40$  the constant is:  $k=40/\log(5)=57$

CEA50-1N



Weber-Fechner law in CIE 230:2019 for threshold colour differences of surface colours and two ranges:  $0.2 < L_r < 1$  and  $1 < L_r < 5$

The Weber-Fechner law describes the lightness  $L^*$  as logarithmic function of  $L_r$ . The Weber-Fechner law describes the lightness  $L_{\text{CIELAB}}$  as potential function of  $L_r=L^*/100$ . IEC 61966-2-1 uses a similar potential function  $L_{\text{CIE}}=m \cdot L_r^{1/2.4}$ .

The Weber-Fechner law is equivalent to the linear equation:  $AL_r=c \cdot L_r$  [1]

Integration leads to the logarithmic equation:  $L^*=k \log(L_r)$ , [2]

Derivation leads for  $AL_r=1$  to the linear equation:  $L_r/\Delta L_r=k=57$ . [3]

For colours in offices the standard contrast range is 25:1-90:3.6.

Table 1: CIE tristimulus value Y, luminance L, and lightnesses L\*

Colour (matte) Tristimulus value Y office luminance relative luminance CIE lightness relative lightness

(contrast) 25:1-90:3.6) Y L  $L_r=L/L_u$   $L^*_{\text{CIELAB}}$   $L^*$   $=k \log(L_r)$

White W (paper) 90 142 5 94 40  $=k \log(5)$

$\approx 18^{\circ}5$   $\approx 28.2^{\circ}5$  5  $\approx 50+44$   $=k \log(5)$

Grey Z (paper) 18 28.2 1 50 0  $=k \log(1)$

Black N (paper) 3.6 5.6 0.2 18 -32  $=k \log(0.2)$

$\approx 18^{\circ}5$   $\approx 28.2^{\circ}5$  0.2 18 -32  $=k \log(0.2)$

For the two lightness ranges it is  $k_1=-32/\log(0.2)=46$  and  $k_2=44/\log(5)=63$ .

line element of Stiles (1946) with „color values“  $L_P, M_D, S_T$

three separate color signal functions

$$F(L_P) = i \ln(1 + 9 L_P)$$

$$F(M_D) = j \ln(1 + 9 M_D)$$

$$F(S_T) = k \ln(1 + 9 S_T)$$

Taylor-derivations:

$$\Delta F(L_P, M_D, S_T) = \frac{dF}{dL_P} \Delta L_P + \frac{dF}{dM_D} \Delta M_D + \frac{dF}{dS_T} \Delta S_T$$

$$= \frac{9i}{1+9L_P} \Delta L_P + \frac{9j}{1+9M_D} \Delta M_D + \frac{9k}{1+9S_T} \Delta S_T$$

CEA51-1N

functions  $q[k(u-u_0)]$

„achromatic signal“-description

with  $u=\log L$  ( $L$ =luminance)

$u_0=\log L_u$  ( $L_u$ =surround luminance)

$$q[k(u-u_0)] = 1 + 1/\sqrt{2} e^{k(u-u_0)}$$

function values:

$$q[k(u-u_0) \rightarrow +\infty] = 1$$

$$q[k(u-u_0) = 0] = \sqrt{2}$$

$$q[k(u-u_0) \rightarrow -\infty] = 2$$

CEA51-3N

„achromatic signal“ discrimination as function of relative light density  $h=\ln H=k(u-u_0)$ ,  $\ln$  = natural log.

$$Q' = \frac{d}{dH} [1 \{ 1 + 1/(1 + \sqrt{2}H) \}] / \ln \sqrt{2}$$

$$= -\sqrt{2} / [\ln \sqrt{2} (1 + \sqrt{2}H) (2 + \sqrt{2}H)]$$

function values:

$$Q'[k(u-u_0) \rightarrow +\infty] = 0$$

$$Q'[k(u-u_0) = 0] = -0.5$$

$$Q'[k(u-u_0) \rightarrow -\infty] = 0$$

CEA51-5N

double line element of Richter (1987) for the lighting technology with the luminance  $L=f(L_P, M_D, S_T)$

$$F(L) = \int_{-\infty}^L (L/\Delta L) dL \quad (\text{relative } L, M, S?)$$

$$F(L) = i Q(H) = \begin{cases} \frac{i}{\bar{k}} Q(\underline{H}) & (u < u_0) \\ \frac{i}{\bar{k}} Q(\bar{H}) & (u \geq u_0) \end{cases}$$

with:  $\underline{k}=1.4$   $\bar{k}=1$   $i=1$   $\bar{i}=-2$

$u=\log L$   $u_0=\log L_u$   $\underline{H}=e^{k(u-u_0)}$ ,  $\bar{H}=e^{-k(u-u_0)}$

$H=e^{k(u-u_0)}$ ,  $\underline{H}=e^{-k(u-u_0)}$ ,  $\bar{H}=e^{-k(u-u_0)}$

CEA51-7N

line element of Vos&Walraven (1972) with „color values“  $L_P, M_D, S_T$

three separate color signal functions

$$F(L_P) = -2i\sqrt{L_P}$$

$$F(M_D) = -2j\sqrt{M_D}$$

$$F(S_T) = -2k\sqrt{S_T}$$

Taylor-derivations:

$$\Delta F(L_P, M_D, S_T) = \frac{dF}{dL_P} \Delta L_P + \frac{dF}{dM_D} \Delta M_D + \frac{dF}{dS_T} \Delta S_T$$

$$\Delta F(L_P, M_D, S_T) = \frac{i}{\sqrt{L_P}} \Delta L_P + \frac{j}{\sqrt{M_D}} \Delta M_D + \frac{k}{\sqrt{S_T}} \Delta S_T$$

CEA51-2N

„achromatic signal“-description

functions  $Q_{1m}[k(u-u_0)]$

with  $u=\log L$  ( $L$ =luminance)

$u_0=\log L_u$  ( $L_u$ =surround luminance)

$$Q_{1m}[k(u-u_0)] = \frac{l}{\ln \sqrt{2}} \ln q[k(u-u_0)] - m$$

function values with  $l=m=1$ :

$$Q[k(u-u_0) \rightarrow +\infty] = -1$$

$$Q[k(u-u_0) = 0] = 0$$

$$Q[k(u-u_0) \rightarrow -\infty] = 1$$

CEA51-4N

luminance discrimination possibility  $L/\Delta L$  as function of  $H$

with:  $L=10^u$   $H=e^{-h} \log e k(u-u_0)$

$dL/du = \ln 10 L$   $dH/du = k H$

it follows:  $L/\Delta L = [kH/(dH \ln 10)]$

$$\frac{L}{\Delta L} = \text{const } H / [(1 + \sqrt{2}H)(2 + \sqrt{2}H)]$$

$Q'[k(u-u_0) \rightarrow +\infty] = 0$

$Q'[k(u-u_0) = 0] = \text{maximum}$

$Q'[k(u-u_0) \rightarrow -\infty] = 0$

CEA51-6N

double line element of Richter (1987) for the lighting technology with the luminance  $L=F(L_P, M_D, S_T)$

$$F(L) = \int_{-\infty}^L (L/\Delta L) dL \quad (\text{relative } L, M, S?)$$

$$F(L) = i Q(H) \quad H=e^{k(u-u_0)}$$

$$Q(H)=[\ln\{1+1/(1+\sqrt{2}H)\}]/\ln\sqrt{2}-1$$

Taylor-derivations:

$$\Delta F(L) = \frac{dF}{dL} \Delta L = i \frac{dQ}{dH} \Delta H$$

$$= -i\sqrt{2}\Delta H / [\ln\sqrt{2}(1+\sqrt{2}H)(2+\sqrt{2}H)]$$

CEA51-8N

